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# **1** On the sensitivity of modelled groundwater recharge estimates to rain gauge

# 2 network scale

4	Andrew J. Wiebe <sup>*</sup> and David L. Rudolph
5	Department of Earth and Environmental Sciences, University of Waterloo, 200 University
6	Avenue West, Waterloo, Ontario, N2L 3G1, Canada
7	
8	* Corresponding author: Tel. +1 519 888 4567
9	E-mail addresses: ajwiebe@uwaterloo.ca (A.J. Wiebe), drudolph@uwaterloo.ca (D.L. Rudolph)
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## 20 Abstract

21

22 Rainfall is often the largest component of the water budget and even a small uncertainty 23 percentage may lead to challenges for accurately estimating groundwater recharge as a calculated 24 residual within a water budget approach. Watersheds are a common scale for water budget 25 assessment, and rainfall monitoring networks typically have widely spaced gauges that are 26 frequently outside the watershed of interest. The effects of rainfall spatial variability and 27 uncertainty on groundwater recharge estimates have received little attention and may influence 28 water budget-derived recharge estimations. In the present study, the influence of spatial density 29 in rainfall measurement on the numerical estimation of groundwater recharge was investigated 30 through a series of modelling scenarios utilizing field data obtained from progressively denser 31 rain gauge networks associated with a typical watershed in southern Ontario. The uncertainty of the recharge component of the water budget was used as a metric to aid interpretation of results. 32 33 The scenarios employed networks composed of: 1) one nearby national weather station (within 3 34 km), 2) a regional network of six stations (within 30 km), and 3) a local network of six stations, 35 five of which were within the selected watershed. A coupled and fully distributed hydrologic 36 model (MIKE SHE) was used in the scenario analysis and applied to the Alder Creek watershed 37 on the Waterloo Moraine near Kitchener-Waterloo, Ontario. Rainfall showed poor spatial 38 correlation, even at the daily time scale. Average annual results over a three-year period showed 39 that recharge rates varied up to 140 mm per year ( $\sim$ 40 % of previously estimated annual 40 recharge) among scenarios, with differences between scenarios greater than the water budget 41 uncertainty during one of the years. These findings suggest that the availability of local rainfall

42 measurements has the potential to influence the calibration of transient watershed43 hydrogeological models.

44

## 45 **1.0 INTRODUCTION**

46

47 The estimation of groundwater recharge is a challenging task at any scale of consideration. With 48 the emergence of regional scale groundwater models, often applied at a watershed scale, the 49 seasonality and spatial variability of recharge has become a hydrologic component of significant 50 importance. This is particularly the case when considering its role as a forcing function in water 51 budgets and contaminant transport processes. Recharge magnitude and distribution is frequently 52 estimated by numerical models that employ a water balance approach, where the magnitude of 53 the recharge is calculated as a residual of the other measured or estimated components of the 54 overall water budget (Healy, 2010). The calculated recharge distributions are then used as 55 boundary conditions in modelling exercises related to watershed-scale assessments of water 56 resources, regional impacts of non-point source contaminants, and changing land-use impacts. 57 The rainfall data that are required for the water budget estimations are often derived from local 58 weather stations that vary in spatial proximity to the study area.

While the scales at which rainfall measurements are made are known to influence their spatial accuracy over regional scales, the impact of measurement density on the spatial distribution of calculated groundwater recharge rates has received little attention (Hess et al., 2016; Sapriza-Azuri et al., 2015; Villarini et al., 2008; Winter, 1981). In many environments, precipitation (P) tends to be the largest component of the water budget (Dingman, 2015). Thus, small percentage uncertainties associated with P will lead to large magnitudes of uncertainty for smaller components of the overall hydrologic flow system – such as groundwater recharge or discharge – that are often estimated as residuals of the total water budget (Thodal, 1997; Wiebe et al., 2015; Winter, 1981). The optimal measurement scale required for rainfall measurements to ensure a particular degree of confidence in the estimation of groundwater recharge for a particular area is largely unknown and dependant on local conditions.

70 Many studies focused on the spatial variation of rainfall and the uncertainty associated 71 with a particular network density have been undertaken to illustrate the significance of 72 precipitation measurement (e.g., Dingman, 2015; Hess et al., 2016; Huff, 1970; Huff and 73 Schickedanz, 1972; Linsley and Kohler, 1951; Villarini et al., 2008; Winter, 1981). The impact 74 of spatial rainfall variability on streamflow has also been addressed, and it is well known that the 75 number of rain gauges and their locations impact the accuracy of modelled hydrographs (e.g., 76 Andréassian et al., 2001; Bell and Moore, 2000; Faurès et al., 1995; Obled et al., 1994; Zhao et 77 al., 2013). Villarini et al. (2008) found that spatial correlation among rain gauges tends to 78 increase, and spatial sampling errors tend to decrease, for increasing data accumulation times 79 (e.g., 15 min, hourly, and daily). The authors do note, however, that the transferability of specific 80 rainfall uncertainty results to other areas may not be directly applicable due to local site 81 conditions.

Previous numerical studies addressing the influence of spatial rainfall variability on recharge have identified that interpolation techniques and the model's spatial grid size are important factors. Mileham et al. (2008) used a semi-distributed, soil-water budget model for a humid, tropical watershed in Uganda (2,098 km<sup>2</sup>) over 15 years and found that cumulative recharge estimates differed by a factor of about 1.5 between a scenario interpolating precipitation

87 via Thiessen polygons and one using inverse distance weighting with 20 rain gauges. Sapriza-88 Azuri et al. (2015) used a fully distributed model with stochastic rainfall distributions generated 89 from rain gauges at 151 weather stations and found that recharge estimates varied based on the 90 scale of the interpolated rainfall data (2.5 km by 2.5 km, or 50 km by 50 km, or lumped over the 91 entire 16,000 km<sup>2</sup> watershed). Applying rainfall at the smallest grid cell size over four decades 92 resulted in 1.5 to 2 times the recharge estimated when rainfall was applied at the other two 93 scales. Recommendations for both the spatial density of observation points and selection of grid 94 sizes for model input are needed for other geographical contexts.

95 Precipitation is frequently measured by rain/snow gauge networks, and ground-based 96 radar methods rely on these for calibration (e.g., Dingman, 2015). The density of Canada's rain 97 gauge network is less than 1 gauge per stream watershed in southern Ontario, where watersheds are on average about 300 km<sup>2</sup> in size (Adam and Lettenmaier, 2003; OMNR, 2007; OMNRF, 98 99 2016). Extreme summer rainfall events in this area may occur over 100 km<sup>2</sup> (Paixao et al., 2015), 100 and convective summer storms can be as small as 5 to 8 km<sup>2</sup> in size (Singh, 1992; Tsanis and 101 Gad, 2001). Such events could easily evade detection by existing rain gauge networks, and these 102 may become increasingly important due to climate change (Collins et al., 2013; Cubasch et al., 103 2001; Jyrkama and Sykes, 2007). This is a potential concern for groundwater recharge estimation 104 under both long-term and event-based conditions. The sustainable management of integrated 105 water supplies depends on accurate quantitative estimates derived from precipitation 106 measurements. Accurate precipitation estimates are also essential for assessing regional-scale 107 water quality vulnerability related both to non-point contaminants and local, extreme hydrologic, 108 event-based conditions near critical receptors such as public supply wells (e.g., Christie et al., 109 2009; the May 2000 Walkerton tragedy – O'Connor, 2002).

110 The objective of the present study was to assess the spatial correlation among point 111 rainfall measurements, and to explore the sensitivity of modelled recharge estimates to spatial 112 variations in rainfall in the vicinity of a typical watershed in southern Ontario. The watershed 113 selected for this study represents watersheds where municipal water sources rely on glacial 114 moraine aquifers, and agricultural activities and urban expansion present challenges related to 115 water quality and quantity. It was hypothesized that recharge estimates in scenarios employing 116 different rainfall networks' interpolated data would differ to a degree that could significantly 117 impact regional water management decisions. The uncertainty associated with the recharge 118 component of a near-surface water budget was employed as a metric of significance. Differences 119 in recharge between scenarios were assessed based on: 1) visual analysis of the spatial 120 distributions of total recharge, 2) the frequency of cell-by-cell differences in modelled total 121 recharge, and 3) changes in water budget components such as cumulative streamflow. Three 122 different spatial scales of rain gauge networks were used for the assessment: i) one national 123 station located within 3 km of the watershed, ii) six regional stations within 30 km of the 124 watershed, and iii) six local stations, five of which were within the watershed. The sensitivity 125 was addressed by comparing the magnitude and spatial distribution of recharge results from three 126 corresponding scenarios: (1) spatially uniform rainfall from the national network, and spatially 127 variable rainfall interpolated from the (2) regional and (3) local networks. Spatially uniform 128 reference evapotranspiration (ET<sub>o</sub>) derived from the national network station was used for all 129 scenarios, and spatial variations in snowfall were held constant in order to isolate rainfall as the 130 variable of comparison.

For this investigation, field data collected from the local rain gauge network within the
study region over a three-year period were utilized to illustrate natural precipitation variability.

We specifically addressed this relatively short temporal period because this is the time scale at which fully-coupled models may be used in practice by environmental consultants to study the impacts of dynamic hydrological events on city water supply systems (Meyer et al., 2017). There could be different results over a longer time scale.

137

#### 138 **2.0 METHODS**

#### 139 2.1 SITE DESCRIPTION

The Alder Creek watershed (78 km<sup>2</sup>; Figure 1) within the Grand River watershed (6,700 km<sup>2</sup>) is 140 141 located on the regional upland of the Waterloo Moraine (GRCA, 1998). Located adjacent to the 142 cities of Kitchener and Waterloo, ON, this watershed's glacial sands and gravels cover over half 143 of its surficial area and facilitate recharge for about seven municipal well fields operated by the 144 Regional Municipality of Waterloo (Brouwers, 2007; CH2MHILL and SSPA, 2003; OGS, 145 2010). Due to its importance for water supply, the watershed and its surrounding area have been 146 the subject of detailed hydrologic modelling in the past (e.g., CH2MHILL and SSPA, 2003; 147 Martin and Frind, 1998; Matrix and SSPA, 2014a, 2014b; Sousa, Frind, et al., 2013). The 148 availability of extensive subsurface geology data and hydrogeological interpretations derived 149 from previous work in the area provides a valuable foundation for the current modelling 150 exercises within the multi-aquifer system of the Waterloo Moraine (e.g., Bajc et al., 2014; 151 Blackport et al., 2014; CH2MHILL & SSPA, 2003; Martin and Frind, 1998). 152 Total annual precipitation is around 900 mm in this region, varying between 600 and 153 1100 mm at the nearby Environment Canada weather station at Roseville, ON, which is located 154 less than 3 km outside the watershed (Government of Canada, 2019; OMNR, 2007). Actual ET

(AET) for the region has been estimated at generally around 540 mm per year (Sanderson, 1998),
and streamflow is on average around 140 mm per unit area at the gauging station within the
watershed (Figure 1; based on daily data, 1975-2015; WSC, 2017). The average baseflow index
(i.e., the fraction of total streamflow constituted by groundwater baseflow) for this station is
about 0.6, according to quarter-year PART hydrograph separation results (based on daily data,
1966 to 2016; Rutledge, 2007; WSC, 2017).

National network daily precipitation and temperature data were obtained for the Roseville
weather station noted above and shown in Figure 1 (Government of Canada, 2019); this is the
closest national station to the Alder Creek watershed. Rainfall data were recorded using a
Canadian Type B rain gauge (113 mm diameter) at a height of 0.4 m and available on a daily
timescale, while snow depths were manually measured each day and converted to snow water
equivalent using a ratio of 0.1 (Government of Canada, 2013, 2019). Daily maximum and
minimum temperatures were obtained from the Roseville station for ET<sub>o</sub> calculations.

168 Regional network rainfall data were obtained from six stations operated by the Grand 169 River Conservation Authority (GRCA) and shown on the inset map of Figure 1. Rainfall data 170 were available at an hourly time scale from a network of tipping-bucket gauges installed for the 171 purposes of flood forecasting (GRCA, 2017a; Shifflett, pers. comm., 2018).

Local network rainfall data were obtained from the Alder Creek field observatory of the
Southern Ontario Water Consortium (SOWC; Wiebe et al., 2019). This network of weather
stations (Figure 1) employed tipping bucket rain gauges (200 mm diameter) recording data every
min. Each of the six gauges was installed at a height of 1 m above the ground surface and
surrounded by an Alter-type wind shield. Data were available for January 2014 onward for all

stations except WS5, where data records began in June 2014. Annual rainfall totals are shown in
Table 1 for each of the three rain gauge networks.

179

## 180 2.2 SPATIAL CORRELATION

181 Spatial correlation for rainfall was assessed using Spearman's rank correlation coefficient for 182 several accumulation times (Gibbons and Chakraborti, 1992; Villarini et al., 2008; Villarini et 183 al., 2010). Each coefficient was generated by comparing the data from a pair of stations. For each 184 accumulation time (1 hr, 3 hr, 24 hr, 1 month), the sum of the data within each time interval of 185 that size was compared. Each correlation coefficient measures the strength of the linear 186 relationship between ranked data at a pair of stations. The Spearman rank correlation coefficient 187 was used instead of the Pearson coefficient because the Pearson method assumes that the data are 188 normally distributed, while the Spearman coefficient does not (Gibbons and Chakraborti, 1992). 189 Rainfall data were assessed for the combined stations of the local and regional networks. The 190 overall time period for this correlation analysis was three years, except for correlations involving 191 station WS5, which employed 2.5 years of data. An exponential model (Villarini et al., 2008) 192 relating the correlation coefficient,  $\rho$ , to the separation distance, h, was employed to fit the data 193 and show general trends in correlation for the different accumulation times (Eqn. 1):

$$\rho(h) = c_1 exp\left[-\left(\frac{h}{c_2}\right)^{c_3}\right].$$
(1)

194

195 The parameters  $c_1$ ,  $c_2$ , and  $c_3$  represent the nugget, correlation distance, and shape factor,

196 respectively (Villarini et al., 2008). Following Villarini et al. (2010) and based on arguments by

197 Krajewski et al. (2003) that a traditional network of rain gauges (one gauge per location) is

198 insufficient to estimate  $c_1$ , a nugget value of  $c_1 = 1.0$  was chosen in all cases. The correlation

199 distance and shape factor for the field data were determined via the Levenberg-Marquardt

algorithm in the scientific computation program GNU Octave (Eaton et al., 2011; Gavin, 2009,

201 2019).

202

### 203 2.3 WATER BUDGET AND UNCERTAINTY

204 Context for the recharge differences between scenarios was portrayed by calculating the 205 uncertainty from an annual vadose zone water budget (Eqn. 2),

$$R = P - AET_{VZ} - Q_{SW} - \Delta S_{VZ}, \tag{2}$$

206

207 where R is recharge, P is total precipitation,  $AET_{VZ}$  is actual evapotranspiration from the vadose 208 zone,  $Q_{SW}$  is the surface water fraction of streamflow (i.e., 1 – baseflow index), and  $\Delta S_{VZ}$  is net 209 storage change in the vadose zone. This water budget assumes that recharge occurring from 210 surface water bodies directly connected to the water table is negligible, i.e., that all recharge 211 migrates through the unsaturated zone. AET derived from the saturated zone is excluded from 212 this water budget because the domain for this budget is the vadose zone; AET derived from the 213 saturated zone has already become recharge (R) and thus should not be counted twice. 214 Uncertainty on recharge ( $\delta R$ ) was calculated under the assumption that the individual 215 uncertainties are independent (e.g., Dingman, 2015) via (Eqn. 3),

$$\delta R = \sqrt{\delta P^2 + \delta A E T^2 + \delta Q^2 + \delta \Delta S_{VZ}^2},\tag{3}$$

216

217

218	(~10%, Kristensen and Jensen, 1975); $\delta Q$ is streamflow uncertainty, (~5%, Herschy, 1973;					
219	Winter, 1981); and $\delta \Delta S_{VZ}$ is uncertainty related to vadose zone storage change, (~5%, assumed					
220	similar to streamflow). Spatial interpolation errors for $P$ and $AET$ were not included. The					
221	uncertainty of the water budget components in Eqn. (3) was calculated using the input data and					
222	sults for a scenario and year with a percentage uncertainty on $R$ that was similar to the average					
223	from all annual simulations, as an example of a typical case.					
224						
225	2.4 NUMERICAL MODEL					
226	The fully distributed MIKE SHE software code (Abbott et al., 1986; Graham and Butts, 2005;					
227	Refsgaard and Storm, 1995) was used to conceptually explore the sensitivity of recharge					
228	estimates to spatial variations in rainfall. This code internally couples the saturated zone (3D),					
229	unsaturated zone (1D), overland flow (semi-distributed), and streamflow (1D) processes, with					
230	surface boundary inputs and outputs such as P and $ET_0$ . The ground surface topography and					
231	seven geological layers for the model were imported from an existing three-dimensional					
232	groundwater flow model (Region of Waterloo Tier Three water budget and risk assessment;					
233	Matrix and SSPA, 2014a) and interpolated onto a grid with 50 m by 50 m cells that composed					
234	the domain for the present study. This included hydraulic conductivity values that had been					
235	calibrated for steady state conditions in the existing model, which used the finite element-based					
236	FEFLOW code (DHI-WASY, 2011). Hydraulic head values from the existing model were					
237	applied at the boundaries of the Alder Creek watershed and specified as the initial conditions					

where  $\delta P$  is precipitation uncertainty, (~10%, Dingman, 2015);  $\delta AET$  is AET uncertainty,

within the domain. The boundary of the domain (Figure 1) was designed to coincide with the
New Dundee dam at the outflow of Alder Lake, about 8 km upstream from the actual outflow of
Alder Creek into the Nith River. This allowed for a well-defined hydraulic head boundary in the
surface water portion of the model. The resulting model domain area was 68 km<sup>2</sup>, and the revised
boundaries adjacent to the dam followed local topographic ridges to the watershed divide
(GRCA, 1998).

244 Precipitation inputs to the model were developed from daily national data, hourly 245 regional data, and 15 min local rainfall data. Rainfall data for the regional and local scenarios 246 were aggregated to the daily time scale and interpolated onto a 250 m by 250 m grid using the 247 inverse distance squared technique. Rainfall data for the national scenario were applied at the 248 daily time scale in a spatially uniform manner. All scenarios employed daily snowfall data from 249 the Roseville station. The model used the average daily air temperature at the Roseville station to 250 calculate the accumulation and melting of snow, based on a modified degree day method (DHI, 251 2017a; Government of Canada, 2019).

252 Drainage of water in the unsaturated zone was represented by the 1D Richards' Equation 253 option (DHI, 2017a). Soil columns for each grid cell were composed of one single soil type 254 corresponding to the surficial soil because the model framework did not allow automated 255 incorporation of the detailed geological layering into the unsaturated zone. Each column was 256 discretized with 0.1 m cells down to 10 m, then 0.2 m cells to 30 m, and then 1 m cells to 55 or 257 80 m depth. The spatial distribution of nine surficial soil types (Figure 2) was based on OGS 258 (2010). Saturated hydraulic conductivity, porosity, and residual moisture content parameters for 259 the van Genuchten curves were based on literature values (D. Graham, pers. comm., 2017; 260 Schaap et al., 1999; Sousa, Jones, et al., 2013), and the n, alpha, and Green and Ampt suction at

the wetting front parameters were selected in order to vary in a conceptually reasonable manner
in comparison with the UNSODA soil types (D. Graham, pers. comm., 2017; Leij et al., 1996;
Table 2). No macropore flow was simulated. The default pressure head values for field capacity
and wilting point (-1 m H<sub>2</sub>O, and -100 m H<sub>2</sub>O, respectively), and the default shape factor for
unsaturated hydraulic conductivity (0.5) were selected based on DHI (2017b) recommendations.

Daily  $ET_o$  inputs to the model were calculated based on the Penman-Monteith method for reference ET, using the UNFAO56  $ET_o$  Calculator (Allen et al., 1998; Raes, 2009). The maximum and minimum daily temperatures at the Roseville station were used to calculate  $ET_o$ for all three scenarios. The "light to moderate winds" option (2 m/s at a height of 2 m above ground surface) was selected to fill in missing wind speed data in the  $ET_o$  calculations.

271 The upper three geological layers that were imported from the existing model were 272 merged into one computational layer for the saturated zone simulation. This ensured that the 273 water table would be present in the uppermost saturated zone cell, improving the stability of the 274 model. The minimum geological layer thickness was set to match the input layers from the 275 existing model (0.1 m). The finite difference option was used to represent flow in the saturated 276 zone (DHI 2017a). Public supply wells within the watershed were incorporated into the model and their average 2008 pumping rates were employed (total extraction: 23,000 m<sup>3</sup>/d; Matrix and 277 278 SSPA, 2014b).

Land use and vegetation data (Figure 3) were compiled from ROW (2010) and from the Ontario Ministry of Natural Resources (OMNR, 2008). The sparse paved areas were not treated specially beyond maintaining an assigned background rooting depth, as required by the model, though the urban areas were assigned a leaf area index (LAI) value representing grass. Maximum

LAI and root depths were obtained from the literature (Canadell et al., 1996; Scurlock et al., 2001). The LAI values for agricultural areas were assigned a linear increase from zero up to the respective literature value for each cell during the month of May; rooting depths linearly increased during the growing season (May to mid-September). LAI was specified to linearly increase for forest areas during May, be held constant during the growing season, and then linearly decrease during the last two weeks of September. No irrigation was included in the model.

Overland flow was represented using a semi-distributed approach via the finite difference method (DHI 2017a). A Manning's *n* value of  $0.3 \text{ m}^{-1/3}$ s was applied throughout the domain to represent the majority agricultural land use with a value for light brush, and detention storage was specified based on literature values for five of the land cover types (Chin, 2006), excluding wetlands and open water.

Stream channels were generated based on the pre-processed (interpolated) model topography to obtain more reasonable agreement between the streamflow and overland flow processes, and cross-sections were generated every 200 m. Manning's *n* values for the channel were based on GRCA (2017b): 0.035 m<sup>-1/3</sup>s for the channel thalweg, and 0.05 m<sup>-1/3</sup>s otherwise.

The model employs independent, automatically adjusted time steps for its overland flow, unsaturated zone, and saturated zone processes (DHI, 2017c; Graham and Butts, 2005).

301 Groundwater recharge is calculated iteratively as an internal flux from the unsaturated zone to

302 the saturated zone during simulations (Graham and Butts, 2005); the accumulated amount for a

303 single cell or the entire watershed was obtained via post-processing.

#### 305 2.5 COMPARISON OF MODEL SIMULATIONS

306 The scenarios were simulated one year at a time for the years 2014 to 2016. The 2014 307 simulations followed a three-year model spin-up period that employed spatially uniform daily 308 rainfall and snowfall data from the Roseville station. Scenarios 2 and 3 were started from the 309 same initial conditions as Scenario 1 in all three years. The method of comparing simulations 310 with different rainfall inputs that start from identical initial conditions has been used in other 311 studies (e.g., Schuurmans and Bierkens, 2007; Sapriza-Azuri et al., 2015). Our study differs from 312 Schuurmans and Bierkens (2007) by focusing on groundwater recharge rather than hydraulic 313 heads and discharge, and from Sapriza-Azuri et al. (2015) by addressing a much smaller watershed (~70 km<sup>2</sup> vs. 16,000 km<sup>2</sup>) using rainfall interpolated from observations within 314 315 different networks rather than stochastic values derived from the overall network. Results from 316 the numerical model were saved on a weekly basis, so each year was represented by 52 weeks 317 during analysis of the simulations. The results were compared based on maps of the spatial 318 distribution of total recharge, the frequency of cell-by-cell differences in total recharge, the 319 visual match between observed and modelled cumulative streamflow, and differences in overall 320 water budget components.

None of the three simulations were calibrated. This study compared the impacts of the different rainfall input data on the precision of the estimated recharge distributions. Each set of input data would result in a different calibrated model, but modifications to the parameters of the model (e.g., hydraulic conductivity values) would obscure the effects of the input data on recharge rates. Using the same starting point for each 52-week simulation allows the differences in recharge rates to be compared for a model domain structure that is identical in all cases (i.e., the same set of hydraulic conductivity values for the geological layers). The comparison of

modelled streamflow for each scenario provides a sense of the degree of calibration that wouldbe required.

Observed and simulated rainfall amounts were compared as follows. The spatial correlation of the numerical model's interpolated rainfall datasets was assessed by selecting 36 uniformly spaced cells from the grid, extracting their precipitation time series, and calculating Spearman correlation coefficients for days with no Roseville snowfall. Days with snowfall were omitted because the observed and simulated daily snowfall amounts differed slightly due to the model's partitioning of rain and snow based on temperature. Rainfall frequency distributions for these 36 cells were also compared with the observed distributions.

337

## 338 **3.0 RESULTS**

339

340 The spatial correlation of rainfall was found to vary substantially at both the regional and local 341 scales. Figure 4 suggests a continuum in the spatial correlation relationships as distance increases 342 from the local to the regional scale. Daily Spearman correlation coefficients ranged between 343 approximately 0.4 and 0.8 (Figure 4). Correlation distances and shape factors for the combined 344 stations of the local and regional networks are shown in Table 3 for different time scales. 345 Correlation distances associated with the fitted curves on Figure 4 ranged from about 90 to 110 346 km. The best-fit curve for monthly coefficients showed lower correlation than the daily curve. 347 Correlation coefficients in the local network were substantially lower than those reported for a dense monitoring network (50 gauges in 135 km<sup>2</sup>, 6 years of data) in the Brue Watershed, SW 348 349 England (Villarini et al., 2008). Daily (Pearson) coefficients were  $\geq 0.85$  in that study, while

these varied between roughly 0.6 and 0.9 for the local network in the present study. The spatial correlation analysis indicates that: 1) rainfall may not be sufficiently uniform temporally and spatially in the region around Alder Creek to justify either reliance upon a single rain gauge to represent the watershed or the neglect of rainfall variation within the watershed itself, and 2) the local network is providing additional rainfall information not captured by the regional network.

The inverse distance squared interpolation technique was found to increase the spatial correlation of the interpolated daily precipitation distributions for the regional and local rainfall scenarios. All Spearman cofficients among 36 uniformly spaced sample points for both Scenarios 2 and 3 were between 0.7 and 1.0, a higher range than observed. Appendix A includes examples of the rainfall interpolation for four representative days with a range of rainfall rates. The interpolated daily rainfall frequency distributions at these 36 points for Scenarios 2 and 3 were similar to those observed within the local and regional networks (Appendix A).

362 A simple, annual water budget for the vadose zone provided a metric for the differences 363 in recharge between scenarios. Figure 5 shows that typical instrument and method uncertainty 364 values on these components lead to a substantial accumulated percentage uncertainty on recharge 365  $(\pm 27\%)$ , prior to accounting for spatial interpolation uncertainties for P or ET. The uncertainty on 366 recharge ( $\delta R$ ) could be at least ±100 mm per year (using Scenario 3 data for 2015; Table 4), with 367 precipitation measurement uncertainty as the largest contributor. Analysis of error for small 368 groundwater components is often disregarded when conducting calibration and water budget 369 uncertainty estimations (Wiebe et al., 2015).

The water budget results from the three scenarios are listed in Table 4, along with other relevant values for the watershed: the observed streamflow totals from the WSC gauge, and a

372 regional, steady state model's estimate of average recharge (M.H. Brouwers, pers. comm., 2017; 373 Matrix and SSPA, 2014a; WSC, 2017). The average total precipitation driving the water budget 374 in the numerical model was different in each of the three rainfall scenarios, and the direction of 375 change from year to year sometimes differed. Table 4 shows that average total precipitation 376 increased from 2015 to 2016 in both Scenarios 1 and 2, while it decreased for Scenario 3. 377 Precipitation differences between scenarios for a given year were up to about  $\pm 20\%$  of the long-378 term average from Roseville. Differences in average recharge varied up to around 140 mm per 379 year, or 44% of average steady state recharge (321 mm; M.H. Brouwers, pers. comm., 2017; 380 Matrix and SSPA, 2014a), although Scenarios 1 and 3 showed nearly equivalent average 381 recharge for 2016. Differences in average recharge with respect to Scenario 3 were greater than 382 the magnitude of the water budget  $\delta R$  for both comparisons in 2014, and for the comparison with 383 Scenario 2 in 2015. Vadose zone AET rates were similar (within  $\pm 11$  mm of Scenario 3) in 2014 384 and 2015; AET for Scenarios 1 and 2 differed from Scenario 3 by +106 mm or +44 mm in 2016, 385 respectively, despite having identical  $ET_0$  input values. This shows a "cascade" effect of the 386 variation of rainfall on other water budget parameters calculated by the numerical model: 387 Differing rainfall inputs can influence AET rates which in turn influence recharge rates. Figure 6 388 shows the spatial distribution of recharge rates for the three rainfall scenarios. Net groundwater 389 discharge conditions are generally present along the Alder Creek channel and tributaries. The 390 2014 maps (a, d, and g) show similar recharge distributions for Scenarios 1 and 2, and higher 391 recharge rates everywhere except near the stream channels for Scenario 3. The 2015 maps (b, e, 392 and h) particularly show differences in recharge rates between different scenarios in the sand and 393 gravel soil types. The 2016 maps (c, f, and i) show similar spatial recharge patterns for Scenario 394 1 and Scenario 3 and lower recharge for Scenario 2, reflecting the lower precipitation in Scenario

395	2 (Table 4). While general spatial differences in recharge rates may be observed in the Figure 6
396	information, Figure 7 presents the frequency of cell by cell differences between scenarios.
397	Despite the similar overall average recharge in the local and national rainfall scenarios in 2016
398	(Table 4), the frequency plot (Figure 7c) shows that this is the result of a balancing of increases
399	and decreases in recharge across the domain. Comparisons involving the local rainfall scenario
400	produced a broader distribution of cell by cell differences in recharge, while the differences
401	between the regional and national scenarios resulted in a more general shift that affected more
402	cells similarly. That is, a greater number of cells changed by differing amounts of recharge when
403	the local rainfall scenario was compared with either of the other two rainfall scenarios.
404	Figure 8 shows that the cumulative streamflow results for the scenario employing local
405	rainfall were closer to the observed streamflow in all three years simulated. Scenario 3
406	streamflow was about 3% lower than the observed cumulative flow at the WSC gauge at the end
407	of 2014, about 10% lower at the end of 2015, and about 20% lower at the end of 2016.
408	Cumulative streamflow results from Scenario 1 were between 25 and 31% lower during the three
409	years, whereas Scenario 2 results were between 27 and 43% lower. Because Scenario 3 provided
410	closer agreement with recorded values in all three years, the local rainfall scenario could be
411	interpreted as requiring less extensive calibration than the other two. However, the baseflow
412	indices at the node representing the WSC gauge were between 0.21 and 0.31 for all scenarios.
413	Scenario 3 had the lowest baseflow values. The model predicted a larger overland flow
414	component of streamflow and much lower baseflow than observed (~0.6; Rutledge, 2007; WSC,
415	2017).

416 Overall, the poor spatial correlation in rainfall near the study area resulted in differences417 in recharge rate estimates for 2014 to 2016 that were largest when the local rainfall scenario was

418 compared with either the regional or national network scenarios. Local rainfall interpolations
419 generally led to recharge and streamflow results that were markedly different than those
420 associated with rainfall from the regional or national networks, suggesting a high degree of
421 sensitivity of recharge rates to the scale of rainfall input data.

422

#### 423 4.0 DISCUSSION

424

425 The results suggest that recharge distributions estimated through numerical modeling can be 426 quite sensitive to the spatial variability of rainfall, as characterized by the spatial correlation 427 analysis. While longer term monitoring followed by modelling would provide a more complete 428 evaluation of the issue, this study suggests that the significant investment required for that 429 research would likely produce non-trivial differences in modelled recharge rates for watersheds 430 similar to Alder Creek for some years. Annual recharge rates could differ by a considerable 431 percentage of the average long-term recharge (e.g., 40%). Local rainfall measurements are 432 frequently unavailable at the scale of watersheds used for public water supply, yet models are 433 frequently used for water management at this scale and in similar settings. The implications of 434 the results are discussed below, following discussion of several aspects of the study itself.

The four main factors that could have influenced the recharge results of this study are: 1) the uncertainty associated with measured rainfall amounts, 2) the frequency of applied rainfall intensities in the model, 3) the increased correlation of rainfall caused by the interpolation method, and 4) the rainfall regimes sampled by the short-term monitoring of the local rainfall network (3 years). First, the accuracy of the readings at the individual rain gauges could

440 influence the interpolated rainfall distribution applied to the model, and therefore recharge. All 441 rainfall measurements are susceptible to human and instrument errors. The local network rain 442 gauges were observed to have instrument errors up to  $\pm 10\%$  on average when tested. The wind 443 screens around the local network's gauges reduce the degree to which wind effects are expected 444 to bias the data, while the regional network likely has a higher level of uncertainty due to 445 infrequent calibration and a typical lack of wind screens. The daily volumetric capture of the 446 Roseville rain gauge was likely to be measured quite accurately, though the wind effects would 447 be different because the gauge type differs from the other two networks.

Second, Mileham et al. (2008) found that the frequencies of interpolated daily rainfall amounts impacted recharge rate estimates. In contrast to the Mileham et al. (2008) study, interpolated daily frequencies of rainfall amounts for the regional and local rainfall scenarios in the present study were similar to each other and to the frequencies observed at the local rain gauges (Appendix A). The lack of noteworthy frequency differences between the interpolated and measured amounts suggests that variations in the rainfall frequency distribution are not a major factor.

Third, recharge rates could have been influenced by the increased spatial correlation of rainfall caused by the inverse distance squared interpolation technique. Interpolation shifted the entire range of Spearman correlation coefficients upward by about 0.2, from about 0.4 to 0.8 for the observed rainfall to about 0.7 to 1.0 for the simulated. Two related issues are: 1) software packages used for fully distributed watershed modelling typically restrict the user to the choice of a small number of interpolation methods, and 2) a more advanced method such as kriging may require a larger number of observation points than are frequently available.

462 Fourth, the short-term nature of data collected by the local rain gauge network may have 463 biased the recharge results by limiting the period of analysis to three years. Thus, the concern is 464 that the limited analysis may not be representative of the actual long-term data. However, the 465 dataset does include two of the types of years that would be desirable in a more extensive study: 466 the rainfall at Roseville in 2016 was essentially equal to the long-term average rainfall over 1973 467 to 2018, and the rainfall in 2014 and 2015 was lower than average (by about 12 and 9%, 468 respectively). Though the recharge modelling is missing a comparative, higher than average 469 rainfall amount for Roseville, the results do suggest that drier years (at the national station) may 470 be more interesting in terms of greater variability in rainfall and recharge (Table 4). While 471 modelling longer-term impacts of the choice of rain gauge measurement network on recharge 472 variability would be preferable, the purpose of present study was to conduct an initial assessment 473 and suggest whether investments in local rainfall monitoring might improve confidence in 474 groundwater recharge estimates.

475 The results of this study have implications for the calibration of hydrogeological models, 476 and therefore implications for the delineation of wellhead protection areas (capture zones), the 477 estimation of groundwater contribution areas for stream reaches, the quantification of the 478 groundwater volume available for long-term extraction, and the assessment of contaminant 479 loadings and transport. The results also provide advice on hydrological monitoring investments. 480 While boundary conditions such as spatial variation in rainfall rates could be estimated during 481 the calibration process (e.g., Anderson and Woessner, 1992), it is common in practice to apply 482 whatever precipitation data are available to fully distributed models and focus calibration efforts 483 on modifying hydraulic conductivity values in order to match observed hydraulic heads and 484 streamflow (Kampf and Burges, 2010). This is a potential concern. In either transient or steady

485 state calibration, a lack of precision in the rainfall distribution will be compensated for by 486 adjustments of the hydraulic conductivity and other soil parameters, potentially mis-representing 487 the actual geology and biasing infiltration and drainage rates. Steady state models would be 488 unable to incorporate repeating rainfall patterns that may exist at small scales without being 489 captured by existing national networks. Such patterns could be caused by trends in wind 490 direction and rainfall distributions associated with evaporation from large lakes (Dingman, 2015) 491 or a heat-island effect near cities (Renard, 2017). The sustainable management of groundwater 492 resources could be impaired by water budget errors related to the precision of rainfall data. For instance, a recharge uncertainty of  $\pm 100$  mm (Figure 5) over the 68 km<sup>2</sup> model domain in the 493 494 present study is roughly equivalent to  $\pm 50\%$  of the adjacent City of Kitchener's (population ~ 495 230,000) annual groundwater extraction (Matrix and SSPA, 2014b).

The magnitude and spatial distribution of recharge is a significant uncertainty for steady state capture zone delineation (Sousa, Frind, et al., 2013). This would be further pronounced for transient capture zones (e.g., Graham and Butts, 2005). Precise rainfall measurements could also affect the recharge rates used to delineate areas of groundwater contribution for stream reaches, which could be an important aspect of land use planning and low impact development strategies aimed at maintaining baseflow to streams (e.g., Chow et al., 2016).

502 Contaminant loadings and transport depend on accurate recharge rates. Recharge 503 distributions also affect the flowpaths of contaminants to receptors such as wells and wetlands 504 and their associated reaction potential (e.g., Loschko et al., 2016). In addition to the potential 505 amount of dilution experienced by contaminants based on recharge rate variation due to the 506 rainfall input data employed, the estimation of dispersion coefficients could also be affected (Yin 507 et al., 2015). Factors such as rainfall amounts, timing, and intensity that could influence recharge

rates have been found to influence pesticide leaching rates in the vadose zone (Isensee andSadeghi, 1995; Sadeghi and Isensee, 1994).

510 Spatial correlation information for rainfall could be used to enhance groundwater 511 modelling. Correlation statistics could guide the design of rainfall monitoring networks used to 512 collect model input data. Comparison of the spatial correlation coefficients for rainfall in the 513 Brue watershed (Villarini et al., 2008) and the Alder Creek watershed suggests that Alder Creek 514 requires relatively more rainfall observation points to capture the spatial variability over small 515 distances (< 15 km). Correlation could also be used to interpret how well sparse rainfall 516 observation stations represent an area, or discrepancies between sparse rainfall data and water 517 table responses.

518 While long-term, high quality records at national weather stations such as Roseville are 519 invaluable, watershed studies at shorter time-scales (transient as opposed to steady state) in 520 certain regions are likely to benefit from more spatially precise rainfall data. The results of the 521 present study suggest that the scale of available data could bias hydraulic conductivity values as 522 calibration compensates for a lack of precise rainfall observations, thus mis-representing 523 recharge and discharge in the near-surface environment. Increasing the density of rain gauges 524 may also be the most cost-effective way to reduce uncertainty associated with recharge 525 estimates, when compared with the cost of collection of subsurface information at the point 526 scale, such as drilling more wells, analyzing soil samples, and conducting hydraulic tests.

527

## 528 5.0 CONCLUSIONS

530 The results of this study indicate that rain gauge network scale can have a significant impact on 531 recharge rate estimates at the watershed scale during short (annual) time scales. Daily Spearman 532 spatial correlation coefficients between gauges of the local and regional networks were typically 533 < 0.8. These correlations show that rainfall is not uniform in the vicinity of the Alder Creek 534 watershed. Simulation of the three rainfall networks resulted in differences in overall average 535 recharge of up to 140 mm, or around 40% of previously estimated steady state recharge (M.H. 536 Brouwers, pers. comm., 2017; Matrix and SSPA, 2014a). Differences in recharge rates between 537 the scenario employing local rainfall and each of the other two rainfall scenarios were more 538 variable than comparisons between the national and regional scenarios, and cumulative 539 streamflow for the local rainfall scenario visually appeared to provide a closer match with 540 observed streamflow. The overall conclusion is that in a setting such as the one described by the 541 observed ranges of local and regional spatial rainfall correlation coefficients, fully distributed, 542 transient models may frequently be compensating for actual rainfall inputs via adjustment of 543 hydraulic conductivity values during calibration. This is a concern for land use planning with the 544 goal of maintaining baseflow to streams, for long-term water resources projections, for 545 representing transient hydrological events, and for contaminant transport models that rely on 546 accurate recharge rate estimates.

547 Future work should address the impact of radar rainfall data and snowfall distributions on548 recharge estimates at the watershed scale.

549

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567

### 568 APPENDIX A

569

570 One supplementary information file contains: a brief description of one additional model 571 scenario, examples of the interpolated rainfall distributions, and a comparison of observed and 572 modelled rainfall frequency distributions.

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## Tables

		Rainfall				
Weather Station	2014	2015	2016			
WS2	987	839	371			
WS3	794	784	797			
WS4	892	853	665			
WS5	$N/A^{\dagger}$	725	746			
WS6 <sup>‡</sup>	800	927	414			
WS7	560	673	789			
Wellesley <sup>§</sup>	849	690	888			
Baden <sup>§</sup>	731	626	537			
Laurel Creek <sup>§</sup>	701	612	605			
Cambridge <sup>§</sup>	677	464	747			
Paris <sup>§</sup>	597	759	892			
Burford <sup>§</sup>	432	641	329			
Roseville <sup>**</sup> (755)	665	689	746			

Table 1. Annual rainfall<sup>\*</sup> (mm) recorded at stations of the local, regional, and national networks.

\* Snowfall data are not included. Roseville snowfall amounts were 183 mm, 111 mm, and 153 mm for 2014, 2015, and 2016, respectively (Government of Canada, 2019).

<sup>†</sup>N/A – not available. WS5 data collection started in June 2014. Jun to Dec 2014: 600 mm.

<sup>‡</sup> The rainfall time series at WS6 is a composite from two gauges at this station.

<sup>§</sup> Grand River Conservation Authority weather station (GRCA, 2017a).

\*\* Environment Canada Weather station (Government of Canada, 2019). The amount in brackets is the average rainfall from 1973 to 2018.

Soil Unit	K <sub>sat</sub> *	$\theta_{sat}^{**}$	$\theta_{res}^{***}$	$\mathbf{n}^{\dagger}$	$lpha^{\dagger\dagger}$
Soli Unit	(m/s)	(-)	(-)	(-)	(cm <sup>-1</sup> )
Outwash gravel	5x10 <sup>-4</sup>	0.28	0.04	4.0	0.040
Ice-contact gravel	3x10 <sup>-4</sup>	0.33	0.04	3.3	0.040
Outwash sand	6.5x10 <sup>-5</sup>	0.43	0.05	3.2	0.035
Ice-contact sand	7x10 <sup>-5</sup>	0.35	0.05	3.3	0.035
Bog/swamp deposits	1x10 <sup>-5</sup>	0.60	0.20	3.0	0.030
Stream alluvium	1x10 <sup>-6</sup>	0.41	0.07	1.5	0.010
Port Stanley Till	5x10 <sup>-6</sup>	0.40	0.06	1.5	0.020
Maryhill Till	1x10 <sup>-6</sup>	0.45	0.06	1.2	0.021
Lacustrine deposits	1x10 <sup>-6</sup>	0.45	0.09	1.3	0.020

Table 2. Unsaturated soil properties (D. Graham, pers. comm., 2017; Leij et al., 1996; Schaap et al., 1999; Sousa, Jones, et al., 2013).

\*  $K_{sat}$  = saturated hydraulic conductivity

\*\*  $\theta_{sat}$  = saturated moisture content

- \*\*\*  $\theta_{res}$  = residual moisture content
- <sup>†</sup> n = van Genuchten fitting parameter
- <sup>††</sup>  $\alpha$  = inverse air entry pressure for van Genuchten curve

Notwork	Method	Time scale	Nugget	Correlation Distance	Shape Factor
Network			(c <sub>1</sub> ; -)	(c <sub>2</sub> ; km)	(c <sub>3</sub> ; -)
	Spearman	1 hr	1.0	88.4	0.21
Local with		3 hr	1.0	113.3	0.24
Regional		24 hr	1.0	91.2	0.39
		1 month	1.0	87.5	0.27

Table 3. Fitting parameters for the spatial correlation best-fit curves.

Year	Componer	nt	Scenario		0
			1	2	3
	Precipitation	849	895	1048	
	Evapotranspiration*	392	376	381	
	Overland Runoff <sup>†</sup>		91	96	124
2014	Storage change <sup>‡</sup>		-53	-33	-20
	Recharge <sup>§</sup>	421	456	562	
	Streamflow at node representing	107	112	148	
Year 2014 2015 2016 Recha	Total Streamflow <sup>††</sup>		121	127	157
	Precipitation	789	714	897	
	Evapotranspiration*		425	421	428
	Overland Runoff <sup>†</sup>	68	61	85	
2015	Storage change <sup>‡</sup>	7	-9	20	
	Recharge <sup>§</sup>	288	241	364	
	Streamflow at node representing	84	75	101	
	Total Streamflow <sup>††</sup>	97	88	116	
	Precipitation	879	756	771	
	Evapotranspiration*	444	382	338	
	Overland Runoff <sup>†</sup>	78	64	93	
2016	Storage change <sup>‡</sup>	13	25	-10	
	Recharge <sup>§</sup>	344	285	349	
	Streamflow at node representing	96	79	112	
	Total Streamflow <sup>††</sup>	107	91	122	
Recharge Estimate from Previous Stud		ly (Tier Three <sup>‡‡</sup> )	321		
		2014	153		
Stre	eamflow estimates from WSC gauge <sup>§§</sup>	2015	112		
	00	2016			

Table 4. Numerical model water budget results and comparisons (results in mm per m<sup>2</sup> per yr).

\* AET excluding AET from the saturated zone. Total AET values were: 493, 476, and 496 mm for Scenarios 1 to 3 for 2014; 521, 505, and 533 mm, respectively, for 2015; and 540, 466, and 439 mm, respectively, for 2016.

<sup>†</sup> Overland flow into stream.

<sup>‡</sup> Includes storage change (unsaturated, snow, and overland flow zones), and boundary flows out of the unsaturated zone (~5 mm/yr/scenario). Boundary flows into the unsaturated zone: 0 mm.

<sup>§</sup> Recharge can be calculated via Eqn. (3).

\*\* Area above gauge =  $47.4 \text{ km}^2$  (WSC, 2017).

<sup>††</sup> Area of model domain =  $68.2 \text{ km}^2$  (GRCA, 1998).

<sup>‡‡</sup> Annual results from calibrated, steady state, saturated zone FEFLOW simulation for Regional Municipality of Waterloo Tier Three Assessment (M.H. Brouwers, pers. comm., 2017; Matrix and SSPA, 2014a).

<sup>§§</sup> WSC (2017). The sums here are based on the 52-week periods of the simulations. There were twelve days with missing data at the start of 2016.

## Figures



Figure 1: The Alder Creek watershed, with Environment Canada, GRCA, and SOWC weather station locations (DMTI, 2011; Esri et al., 2019; Government of Canada, 2019; GRCA, 1998, 2017a; WSC, 2017). The Water Survey of Canada (WSC) stream gauging station location is also shown near WS3.



Figure 2: Surficial soils in the model domain (DMTI, 2011; GRCA, 1998; OGS, 2010).



Figure 3: Land use in the model domain (DMTI, 2011; GRCA, 1998; OMNR, 2008; ROW, 2010). The "Agriculture" category includes minor areas of recreation and open land.



Figure 4: Spatial correlation between rainfall measurements for the combined stations of the local and regional networks.



Figure 5: Instrument and method uncertainty for the Scenario 3 (2015) overall, near-surface

water budget.



Figure 6: Recharge estimates for the three rainfall scenarios (GRCA, 1998; DMTI, 2011). Maps show results as follows: Scenario 1 (national), (a) 2014, (b) 2015, and (c) 2016; Scenario 2 (regional), (d) 2014, (e) 2015, and (f) 2016; and Scenario 3 (local), (g) 2014, (h) 2015, and (i) 2016. The local weather stations are shown as black triangles.



Figure 7: Frequency of differences in recharge rates between the three rainfall scenarios. "S3 - S1" implies a cell-by-cell subtraction of Scenario 1 from Scenario 3, etc.



Figure 8: Comparison of cumulative streamflow results for the three simulations with recorded flows at the Water Survey of Canada (WSC) gauge. The WSC gauge was missing 12 days of data at the start of 2016.

## **Appendix A: Supplementary information**

This supplementary information file contains: a brief description of one additional model scenario, examples of the interpolated rainfall distributions, and a comparison of observed and modelled rainfall frequency distributions.

One scenario was considered in addition to the national, regional, and local rainfall scenarios presented. This scenario was conceptualized as a reference scenario in which rainfall was interpolated from the set of all thirteen available rain gauges (Table 1). Interpolations were made at the daily time scale using the inverse distance squared method.

Figure A.1 suggests that the reference scenario results were very similar to those of the local scenario for several larger rainfall events and contain only minor differences. Table A.1 shows the individual stations' readings for these examples. The cumulative streamflow results of the reference scenario were similar to (within about 20 mm per unit area of) the cumulative streamflow results of the regional and national scenarios in 2014, and very similar to (within a few mm per unit area of) those from the local rainfall scenario in 2015 and 2016 (Figure A.2). Results for the water balance components of the reference scenario were intermediate values between the local and regional scenarios' results, but the values were generally closer to the local scenario. This is likely because of the immediate impacts of the local gauges within the watershed through the interpolated precipitation distribution. The minimal differences between the reference scenario and the local rainfall scenario, and the poorer match between the reference scenario does not constitute an improvement with respect to the results of the local scenario.



Figure A.1: Examples of rainfall interpolations for 20 May 2014 (a, b, c), 15 Jul 2014 (d, e, f), 24 Nov 2014 (g, h, i), and 20 Apr 2015 (j, k, l). The first column (a, d, g, j) shows results for the local network, the second column (b, e, h, k) shows results for the regional network, and the third column (c, f, i, l) shows results for the reference scenario (all networks).

		Rainfall			
Weather Station	20-May-14	15-Jul-14	24-Nov-14	20-Apr-15	
WS2	16.8	42.8	35.6	15.8	
WS3	21.2	0.0	42	0	
WS4	0.0	1.6	50.2	15.6	
WS5	N/A	26.0	35.8	14	
WS6	0.0	2.2	41	15.4	
WS7	15.2	0.6	25.6	11	
Wellesley	22	14.6	34.2	17.2	
Baden	0	31.4	39.2	17.2	
Laurel	10	18.6	34.4	20.8	
Cambridge	6.2	0.4	26.2	14.4	
Paris	0.8	0.6	25.6	22.8	
Burford	0	0.6	20.4	19	
Roseville	15.2	0	3.7	0.6	

Table A.1. Daily rainfall (mm) on the four days portrayed in Figure A.1 (GRCA, 2017a; Government of Canada, 2019).



Figure A.2: Cumulative streamflow results from all scenarios including the reference scenario.

Figure A.3 shows the simulated and observed rainfall frequencies for depths less than 20 mm. The simulated frequencies tend to be similar or slightly higher than the observed regional and local values. The simulated frequencies follow the same pattern as the local and regional frequencies, unlike what was observed during spatial rainfall distribution analysis by Mileham et al. (2008), where the simulated and observed frequency patterns differed to a greater extent.



Figure A.3: Frequency distributions of observed and simulated daily rainfall: a) log scale for frequency, b) linear scale for frequency (Government of Canada, 2019; OMNR, 2007; GRCA, 2017a; Wiebe et al., 2019). The simulated rainfall time series were extracted from 36 grid cells for both the regional and local rainfall scenarios.